



IMAGE HEATING APPARATUS AND  
HEATER USED IN THIS APPARATUS

BACKGROUND OF THE INVENTION

5 Field of the Invention

The present invention relates to a heater particularly effective if it is used in a fixing apparatus of an image forming apparatus such as a copier or printer, and to an image heating apparatus using this heater.

Related Background Art

For convenience' sake, an image heating fixing apparatus as an example of a heating apparatus will be described.

15 In an image forming apparatus such as a copier, printer, or facsimile, an image heating fixing apparatus is a heating apparatus for heating/fixing-processing, on a recording material surface, an unfixed toner image corresponding to image information formed on the surface of a recording material (electro fax sheet, electrostatic recording sheet, transferring material sheet, print paper, or the like) in a direct or indirect (transferring) system using toner made of a thermomeltable resin or the like by proper image forming process means such as electrophotography, electrostatic recording, magnetic recording, or the like.

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Conventionally, for such an image heating fixing apparatus, a heat roller system has been widely used.

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The heat roller system is a system which has a basic construction comprising a metallic roller provided  
5 therein with a heater, and a pressure roller having an elasticity and pressure-contacted to said roller, and in which, by passing a recording material through a fixing nip portion formed by one pair of these rollers, an unfixed toner image bore on said recording material  
10 is heated and pressurized to fix.

However, in the above heat roller system, since the heat capacity of the roller is large, very much time was required for raising the roller surface to a desired fixing temperature. Besides, for this reason,  
15 for quickly executing an image output operation, there is a problem wherein the roller surface must be  
temperature-adjusted to a temperature in a certain extent even when a machine is not used.

One improved and devised on that point is  
20 disclosed in Japanese Patent Application Laid-open No. 10-293490. This is composed by an insulating layer and a heat generation layer are laminated on a surface of a metallic roller. Such a roller is difficult in manufacture, besides, since a contact point for  
25 supplying an electric power to the roller slides, problems such as generation of noise and a short duration arise, so it does not reach a practical use in

practice.

So, the present applicant has proposed before a  
heating apparatus of a film heating system (for  
example, see Japanese Patent Application Laid-open No.  
5 63-313182, Japanese Patent Application Laid-open No. 2-  
157878, Japanese Patent Application Laid-open No. 4-  
44075, and Japanese Patent Application Laid-open No. 4-  
204980.

This film heating system is a system in which a  
10 heating body and a heated material are put into close  
contact with one surface side and the other surface  
side of a heat-resisting film, respectively, and the  
thermal energy of the heating body is given to the  
heated material through the heat-resisting film, and a  
15 heating apparatus of an on-demand type in which members  
of low heat capacity can be used for the heating body  
and film, there is quick startability, and the power  
consumption in standby is considerably small, can be  
constructed.

20 FIGS. 12A to 12C show one example of a heating  
apparatus of the film heating system. This example is  
an image heating fixing apparatus of the film heating  
system. FIG. 12A is an enlarged cross-section model  
view of a principal part, FIG. 12B is a partially cut-  
25 off plan model view on the surface side of a heating  
body, and FIG. 12C is a plan model view on the back  
surface side of the heating body.

Reference numeral 7 denotes a heating body, which is a slender and thin-plate-shaped member whose  
longitude is a vertical direction to the drawing  
surface of FIG. 12A, entirely low heat capacitive, and  
5 generates heat by being electrified.

Reference numeral 13 denotes a heating body  
support member, whose longitude corresponds to a  
vertical direction to a drawing surface of FIG. 12A,  
being adiabatic and rigid. On the lower surface side  
10 of this support member 13, along the member longitude,  
a seat gouged portion 13a elongating in the  
longitudinal axis and in shallow grooved shape into  
which the above heating body 7 can be fitted is  
comprised, and the heating body 7 is fitted into this  
15 seat gouged portion 13a and supported by the support  
member 13.

Reference numeral 12 denotes a thin heat-resisting  
film and 9 does an elastic pressure roller, the film is  
sandwiched, and the heating body 7 supported by the  
20 support member 13 and the pressure roller 9 are  
pressure contacted with a predetermined pressure force  
to form a fixing nip portion (heating nip portion) N.

The film 12 moves in an arrow direction with close  
contacting the fixing nip portion N to the surface on  
25 the downward facing side of the heating body 7 and  
sliding by a not-shown drive member, or the pressure  
roller 9 being rotation-driven.

And, when a paper leaf body (recording material)  
11 carrying an unfixed toner image 10, as a heated  
material, is introduced between the film 12 of the  
above fixing nip portion N and the pressure roller 9,  
5 the paper leaf body 11 is sandwich-conveyed in the  
fixing nip portion N together with the film 12 and  
heated by heat from the heating body 7 through the film  
12, and unfixed toner 10 is heat-fixed on the paper  
leaf body surface. The paper leaf body 11 passed  
10 through the fixing nip portion N is separated from the  
surface of the film 12 and conveyed.

As the heating body 7, a so-called ceramic heater  
in which a ceramic board having electrical-insulating  
performance, good heat conductivity and heat-  
15 resistivity is used as a heating body board. The  
~~heating body 7 of this example is a ceramic heater.~~

That is, 1 denotes a slender and thin-plate-shaped  
ceramic board.

Reference numeral 2 denotes first and second  
20 parallel two-stripe narrow-band-shape electrification  
heat-generation resistor patterns (one is a first, the  
other is a second) formed and comprised along the board  
longitude on the surface side of this ceramic board 1.

Reference numeral 5 denotes two conductor patterns  
25 (one is a first, the other is a second) as the first  
and second power supply electrodes (electrode contact  
points) formed and comprised with being arranged on the

longitude one end portion side of the ceramic board surface. The first power supply electrode 5 is electrically conducted to one end portion of the first resistor pattern 2 through an extension pattern portion. Besides, the second power supply electrode 5 is electrically conducted to one end portion of the second resistor pattern 2 through an extension pattern portion.

Reference numeral 6 denotes a conductor pattern as a folded-back electrode formed and comprised on the ceramic board surface by electrically conducting between the other end portions of the first and second resistor patterns 2.

Reference numeral 3 denotes a heater surface protective glass layer, which is formed and comprised to cover substantially entirely the heater surface except the portion of the first and second power supply electrodes 5. By this protective glass layer 3, each extension pattern portion of the first and second resistor patterns 2 and the first and second power supply electrodes 5, and the folded-back electrode 6 are protected by being covered.

Reference numeral 4 denotes a temperature sensing element such as a thermistor or the like, which is disposed by being contacted to substantially the center portion in the longitudinal direction on the heater back surface side, that is, the back surface side of

the ceramic board 1.

The surface side having the protective glass layer  
3 of the above ceramic heater 7 is the film sliding  
surface side, and the surface side of this ceramic  
5 heater 7 is exposed to the exterior and fitted in the  
seat gouged portion 13a on the lower surface side of  
said support member 13 and disposed.

Reference numeral 8 denotes a power supply  
connector. By predetermined fitness to the power  
10 supply connector mounting portion of the support member  
13 disposing and supporting the heater 7, first and  
second power supply spring contact points 8a on the  
power supply connector 8 side are pressurized and  
contacted to the first and second power supply  
15 electrodes 5 of the heater 7, and the heater 7 and a  
not-shown power supply circuit are electrically  
connected.

By performing power supply from the power supply  
circuit through the power supply connector 8 to the  
20 first and second power supply electrodes 5, by the  
electrification heat-generation resistor patterns 2  
generating heat throughout the longitude entire length,  
the heater 7 rapidly raises the temperature. And, the  
temperature rising information is converted into  
25 voltage information by the temperature sensing element  
7 disposed on the heater back surface side and  
detected, the output is calculated by a not-shown

control circuit such as CPU or the like, and an AC input from the power supply circuit to the heater 7 is adjusted so that the temperature of the heater 7 is temperature-controlled to a predetermined temperature.

5        In the fixing apparatus adopting such a film heating system, since the film 12 of a low heat capacity and the heater 7 can be used, it becomes possible to shorten a wait time (quick start) as compared with the conventional heat roller system.

10       Besides, since the quick start can be done, pre-heating upon non-print operation becomes unnecessary, and power-saving in a synthetic meaning can be intended.

By the way, as the ceramic heater of the above-described example, the heating body using the ceramic board such as alumina as the board has the problems

15       that the ceramic is fragile, or, the cost is high, it is unsuitable for bending processing or the like, and the like.

So, in Japanese Patent Application Laid-open No. 9-244442, Japanese Patent Application Laid-open No. 10-275671, a heating body (hereinafter, referred to as conductive board heater) in which, by forming an insulating layer on a metal, a board having the same insulation ability as the conventional ceramic board is

20       made, and a resistor pattern, a conductor pattern, and an insulating sliding layer of the uppermost layer are formed thereon is proposed.

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However, in the conductive board heater using metal as the board, since thermal expansion is large, and expansion and shrinkage are repeated in a heating apparatus, there is a defect that the electrode portion to which the power supply spring contact point on the power supply connector side is pressurized and contacted is worn and contact inferior occurs and it is easy to break.

Besides, since the position of the resistor pattern of the heating body varies, excessive heating, insufficient heating, uneven heating at an end portion, or uneven curl unevenness at a paper end is occurred.

#### SUMMARY OF THE INVENTION

The present invention has been made in view of the above problems, and its object is to a heater that can prevent contact defect between an electrode provided in the heater and a connector of an image heating apparatus holding this heater, and an image heating apparatus using this heater.

Another object of the present invention is to provide a heater that can prevent heating defect by thermal expansion of the heater, and an image heating apparatus using this heater.

Still another object of the present invention is to provide an image heating apparatus having:

a heating member for heating an image on a recording material, the heating member having a metallic substrate and heat generating resistor;

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a supporting member for supporting the heating member;

wherein the metallic substrate having a positioning portion for positioning the metallic substrate on the supporting member.

Still another object of the present invention is to provide a heater having:

a metallic substrate;  
a heat generating resistor;

wherein the metallic substrate having a positioning portion for positioning the metallic substrate on the image heating apparatus.

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Still another object of the present invention is to provide a heater having:

a substrate, the substrate having a positioning portion for positioning the substrate on the image heating apparatus;

a heat generating resistor;

wherein the positioning portion is provided in the interior of the substrate.

Further objects of the present invention will become apparent by reading the below detailed description with reference to the accompanying drawings.

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# BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic construction model view of  
one example of an image forming apparatus;

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FIG. 2 is a schematic construction model view of a  
5 fixing apparatus;

FIGS. 3A, 3B and 3C are construction model views  
of a conductive board heater, in which FIG. 3A is a  
view representing a heater surface, FIG. 3B is a view  
representing a heater back surface, and FIG. 3C is a  
10 view representing a heater side surface;

FIG. 4 is an exploded perspective model view of  
the heater and a stay;

FIGS. 5A, 5B and 5C are construction model views  
of another example of a conductive board heater, in  
15 which FIG. 5A is a view representing a heater surface,  
~~FIG. 5B is a view representing a heater back surface,~~  
and FIG. 5C is a view representing a heater side  
surface;

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FIG. 6 is an exploded perspective model view of  
20 the heater and a stay;

FIGS. 7A, 7B and 7C are construction model views  
of a conductive board heater of embodiment 2, in which  
FIG. 7A is a view representing a heater surface, FIG.  
7B is a view representing a heater back surface, and  
25 FIG. 7C is a view representing a heater side surface;

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FIG. 8 is an exploded perspective model view of  
the heater and a stay;

FIGS. 9A and 9B are model views showing shapes upon expansion of the heater in a seat gouged portion of the stay, in which FIG. 9A shows a case of the heater in which positioning means is a board bending portion, and FIG. 9B shows a case of the heater in which the positioning means is a hole;

FIGS. 10A, 10B and 10C are construction model views of a conductive board heater of embodiment 3, in which FIG. 10A is a view representing a heater surface, FIG. 10B is a view representing a heater back surface, and FIG. 10C is a view representing a heater side surface;

FIG. 11 is an exploded perspective model view of the heater and a stay; and

FIGS. 12A, 12B and 12C are illustrative views of a heating apparatus of a film heating system and an example of a ceramic heater, in which FIG. 12A is an enlarged sectional view of a fixing portion, FIG. 12B represents a heater surface, and FIG. 12C represents a heater back surface view.

#### DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

(Embodiment 1)(FIG. 1, FIG. 2, FIGS. 3A to 3C, FIG. 4, FIGS. 5A to 5C and FIG. 6)

##### (1) Example of Image Forming Apparatus

FIG. 1 is a schematic construction model view of one example of an image forming apparatus. The image

forming apparatus of this example is a copier or printer utilizing a transferring type

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electrophotographic process, or a facsimile.

Reference numeral 21 denotes a drum-shape  
5 electrophotographic photosensitive body, which is rotated and driven counterclockwise of an arrow at a predetermined peripheral speed.

Reference numeral 22 denotes a charging roller, which is abutted on the photosensitive body 21 with a  
10 predetermined pressurizing force, and to which a predetermined charging bias is applied from a not-shown power source portion, thereby evenly charging processing the peripheral surface of the rotating photosensitive body 21 to a predetermined polarity and  
15 potential.

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By performing image exposure 23 to the charging processing surface of the photosensitive body 21 by not-shown image exposure means (manuscript image projecting means, laser beam scanner, or the like), an  
20 electrostatic latent image corresponding to an exposure image pattern is formed on the photosensitive body surface. Reference numeral 24 denotes a developing apparatus, in which the electrostatic latent image on the photosensitive body surface is normal-developed or  
25 reverse-developed as a toner image.

Reference numeral 25 denotes a transferring roller, which is abutted on the photosensitive body 21

with a pred termed pressurizing force to form a transferring nip portion. By paper-feeding a transferring material sheet (leaf body) 11 to the transferring nip portion from a not-shown paper feeding portion at a predetermined timing, and applying a predetermined transferring bias to the transferring roller 25 from a not-shown power source portion, toner images on the photosensitive body 21 side are transferred in order to the surface side of the transferring material sheet 11 paper-fed to the transferring nip portion.

The transferring material sheet 11 passing through the transferring nip portion is separated from the photosensitive body 21 surface, conveyed to an image heating fixing apparatus 27, receives heat fixing processing of a carrying unfixed toner image, and paper-discharged.

Besides, the photosensitive body surface after the transferring material sheet separation receives removal of adhering remaining materials such as transferring remaining toner or the like by a cleaning apparatus 26 to be a pure surface, and is repeatedly subjected to image formation.

## (2) Image Heating Fixing Apparatus 27

The image heating fixing apparatus 27 of this example is a pressure roller drive type film heating system heating apparatus. FIG. 2 is a schematic

construction view of the apparatus.

Reference numeral 17 denotes a conductive board heater as a heating body according to the present invention, which is a member slender and thin plate shape with a longitude in a vertical direction to the drawing and wholly low heat capacitive. The structure of this heater 17 will be described in detail in the next item (3).

Reference numeral 13 denotes a heating body support member of a substantially semicircular conduit shape in cross section (hereinafter, referred to as a stay), which is a member having heat resistibility and rigidity. On the lower surface side of this stay 13, along the stay longitude, a slender and bottom shallow groove shape seat gouged portion 13a into which the above conductive board heater 17 is fitted is comprised, and the conductive board heater 17 is fitted into this seat gouged portion 13a and supported by the stay 13.

Reference numeral 12 denotes a cylindrical thin heat-resisting film (fixing film), which is loosely outside-fitted to the stay 13 in which the heater 17 is disposed.

Reference numeral 9 denotes an elastic pressure roller as a pressure rotor. It comprises a core metal 9a, and a rubber elastic layer 9b good in mold release ability such as silicone rubber provided concentrically

with said core metal 9a, and both end portions of the core metal 9a are supported through a bearing between not-shown chassis side plates of the apparatus to be free in rotation, respectively.

5           On the upper side of this pressure roller 9, the above heater 17 is disposed, the stay 13 on which the cylindrical film 12 is outside-fitted is oppositely disposed with the heater 17 side facing downward, a pushing-down force is made to act on the stay 13 by  
10   not-shown biasing means, and the facing-down surface of the heater 17 is pressurized and contacted to the upper surface of the pressure roller 9 with sandwiching the film 12 by a predetermined pressurizing force against the elasticity of the rubber elastic layer 9b.  
15   Thereby, the film 12 is sandwiched between the heater  
~~17 and the elastic pressure roller 9 and a fixing nip~~  
portion N of a predetermined width is formed.

          The pressure roller 9 is rotated and driven clockwise by not-shown drive means at a predetermined  
20   peripheral speed. A rotational force acts on the cylindrical film 12 by the pressure contact frictional force in the fixing nip portion N between the outer surface of said roller and the outer surface of the film 12 by the rotation of this pressure roller 9, and  
25   said film 12 becomes in a rotation state around the outside of the stay 13 with a peripheral speed substantially corresponding to the rotational



peripheral speed to the pressure roller  
counterclockwise of an arrow with its inner surface is  
closely contacted and slid with the facing-down surface  
of the heater 17 in the fixing nip portion N (a  
5 pressure roller drive system).

The stay 13 functions also as a guide member of  
this rotating film 12. Reference numeral 13b (FIG. 4)  
denotes a rib in the film rotation direction provided  
by forming spaces along the longitude on the outer  
10 surface of the side wall portion of this stay 13. By  
the presence of this rib, the sliding resistance  
between the stay side wall portion outer surface and  
the rotation film inner surface is reduced.

Besides, by interposing a lubricating agent such  
15 as heat-resisting grease or the like between the  
~~facing-down surface of the heater 17 and the inner~~  
surface of the film 12, the rotation of the above film  
12 can be made smoother.

In a state wherein the pressure roller 9 is  
20 rotated and driven, attendant upon this, the  
cylindrical film 12 becomes in a rotation state, the  
heater 17 is electrified as described later, and the  
fixing nip portion N rises to a predetermined  
temperature by heat generation of said heater 17 to be  
25 temperature-adjusted, the transferring material sheet  
11 carrying the unfixed toner image 10 is introduced  
between the film 12 of the fixing nip portion N and the

pressure roller 9, and, in the fixing nip portion N,  
the toner image carrying surface side of the

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transferring material sheet 11 comes into close contact  
with the outer surface of the film 12 and sandwich-  
5 transferred in the fixing nip portion N together with  
the film. In this sandwich-transferring process, the  
heat of the heater 17 is given to the transferring  
material sheet 11 through the film 12, and the unfixed  
toner image 10 on the transferring material sheet 11 is  
10 heated, melted, and fixed. After the transferring  
material sheet 11 passes through the fixing nip portion  
N, it is curvature-separated from the outer surface of  
the rotating film 12 and transferred.

(3) Conductive Board Heater 17

15 FIG. 3A is a partially cut-off plan model view on  
the surface side of the conductive board heater 17 of  
this example, FIG. 3B is a plan model view on the back  
surface side, and FIG. 3C is a vertical sectional model  
view.

20 This heater 17 forms an insulating glass layer 15  
as a first insulating layer in almost the whole region  
of the surface of a conductive substrate (conductor  
substrate) 16. And, on this insulating glass layer 15,  
substantially similarly with the ceramic heater 7 of

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25 FIGS. 12A to 12C described before, first and second  
parallel two-stripe narrow-band-shape electrification  
heat-generation resistor patterns 2, conductor patterns

5 as first and second power supply electrodes, a conductor pattern 6 as a folded-back electrode, and a heater surface protective glass layer 3 as a second insulating layer are formed and comprised.

5 And, in part of the conductive substrate 16 of said conductive board heater 17, a punch-out processing hole 18a as means for positioning in relation to the stay 13 is provided.

For the conductive substrate 16, metal or the like  
10 such as SUS 430 whose coefficient of thermal expansion is easy to be matched to that of glass, is used. The length of said substrate 16 is desirable to be 270 mm, the width is desirable to be from 5 mm to 15 mm, and the thickness is desirable to be from 0.5 mm to 2 mm.

15 If too thin, a great warp is generated after printing due to the difference in coefficient of thermal expansion and it becomes difficult to assembly.

Besides, if too thick, the heat capacity of the heater becomes large, and, in case of abutting a thermistor or  
20 the like from the back surface, the response is delayed and a desirable control becomes difficult. This causes the generation of image problems such as fixing defect, luster unevenness, and offset.

For having a withstand voltage of 1.5 kV or more,  
25 the insulating glass layer 15 as the first insulating layer is formed into a thickness from 30 microns to 100 microns, and for preventing a pinhole, it is preferable

to take a method of printing a plurality of times.  
Besides, to increase the adhesive performance between  
the conductive substrate 16 and this insulating glass  
layer 15, the conductive substrate 16 is roughing-  
5 processed by sand blast, etching, or the like, and  
after degrease, the insulating glass layer 15 may be  
printed. Since this insulating glass layer 15 serves  
for not only the withstand voltage but also preventing  
the heat generated in the resistor patterns 2 from  
10 escaping to the substrate 16 side, the coefficient of  
thermal conductivity is preferably equal to or less  
than 2 W/m.K.

Further, on this insulating glass layer 15, the  
resistor patterns 2 and the conductor patterns 5, 6 are  
15 printed.

~~Further, as the uppermost layer, the heater~~  
surface protective glass layer 3 is printed as the  
second insulating layer. For this protective glass 3,  
smoothness for slidability with the film 12 is required  
20 and insulating performance and a high thermal  
conductivity (preferably, equal to or more than 2 W/m.K  
or more) are required.

Ones such as the above glass layer, resistor  
patterns, and conductor pattern are made by baking  
25 after printing using screen printing, like the  
conventional ceramic heater.

The punch-out processing hole 18a as the means for

positioning provided in part of the conductive  
substrate 16 of the heater is preferably provided  
within 90 mm from the electrode 5 for power supply.

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Assuming that one having a length of 270 mm as a  
5 heater for A4 size is used at 200°C of the temperature  
upon print, on the basis of the linear coefficient of  
thermal expansion of SUS 430, ( $10.5 \times 10^{-6}/^{\circ}\text{C}$ ), as the  
conductive substrate 16, this is determined from the  
obtained amount of thermal expansion. The thermal  
10 expansion in the heater longitudinal direction in this  
case is calculated by the following expression.

$$(200 - 20)^{\circ}\text{C} \times 270 \text{ mm} \times 10.5 \times 10^{-6}/^{\circ}\text{C} = 0.51 \text{ mm}$$

That is, an extension of about 0.5 mm over the entire  
heater length is calculated.

15 For the resistor patterns 2, a length for  
involving the width 216 mm of letter size is required.

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But, the positions of both ends of this resistor  
patterns 2 are determined by the positional  
relationship in a state of being thermally expanded in  
20 a use temperature.

A holding method of the conventional heater to the  
stay is either fixed or completely free at both ends.

In the former case, by thermal expansion, the  
heater fixing portion becomes a knot and the unfixed  
25 portion becomes a belly, causing the generation of  
unevenness in the pressure distribution. In the latter  
case, the position of the resistor pattern is difficult

to be determined, and the wear of the electrode is intense.

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From this, unless the vicinity of the electrode 5 for power supply of AC of the heater is positioned, friction is generated between the spring contact point 8a of the connector and the electrode 5 every time when being electrified, the electrode 5 is gradually shaved, and finally, a problem that the contact resistance increases, heat is generated, and the electrode is baked and broken, is generated.

From the experience of an alumina heater of 270 mm that does not adhere to the conventional stay 13, the thermal expansion becomes 0.34 mm over the entire length. Considering by distributing this to both sides, up to 0.17 mm, it is thinkable that there is no problem even if there is a shift of the contact point.

Accordingly, for suppressing the movement of the contact point within this 0.17 mm, the distance from the positioning means 18a to the electrode 5 is preferable to be

$$270 \times 0.17 / 0.51 \approx 90 \text{ mm}$$

As the distance from the electrode position, the farthest one from the positioning means 18a of the electrodes 5, which is two, is measured.

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25. If the connector 8 is inserted from the arrow direction of FIGS. 3A to 3C and FIG. 4, in further both the contact electrodes 8a of the connector 8, sliding

friction is reduced and the reliability of conductivity increases.

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FIG. 4 is a view showing the shape of the stay 13 for mounting the heater 17, in which pin-like positioning means 18a' fitting to correspond to the punch-out hole 18a as the positioning means on the heater 17 side is provided on the stay 13. The shape relationship between the positioning portion of the heater and the positioning portion of the stay is interchangeable. Besides, the heater is not adhered to the stay.

For the stay 13, one whose strength is increased by inserting glass in a heat-resisting resin such as PPS, liquid crystal polymer, or phenolic resin, is used. These resins are used by injecting a mold for molding. By manufacturing this mold into a shape for molding into the positioning means 18a', the positioning means 18a' can be made.

Note that the positioning means 18a on the heater 17 side may be not the hole but a boss or emboss.

Or, as shown in FIGS. 5A to 5C, a notch portion 18b on the heater side is used as the positioning means, and the fitting portion of the stay 13 side may be a projection 18b' as shown in FIG. 6.

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The works of the above positioning means 18a and 18a', 18b and 18b' are effective also for accurately disposing the positions of the electrification heat-

generation body patterns 2 of the heater 17 in the fixing nip portion N in relation to the passing position of the transferring material sheet 11 as the heated material. In the conventional ceramic heater, for reducing stress, ones that do not adhere are more. However, since this makes inaccurate the position in the longitudinal direction in the stay interior, in order that the resistor pattern goes out to the exterior of the pressure roller, the dimension in the longitudinal direction of the heating body must have a margin. Since this becomes large as about 2 mm on one side, it is undesirable on cost and for making the apparatus structure small.

However, as this embodiment, if the standards 18a and 18a', 18b and 18b' for positioning are provided on one side, since the positions of the resistor patterns 2 can be accepted within  $\pm 0.4$  mm that is the sum of the fitting tolerance  $\pm 0.1$  mm of this portion and the tolerance 0.3 mm of screen printing, since the accuracy is very good and the heat of the transferring material sheet end portion is given as designed, there is no occurrence of curl and end portion fixing defect.

(Embodiment 2)(FIGS. 7A to 7C, FIG. 8, FIGS. 9A and 9B)

In the heater 17 of this embodiment, as shown in FIGS. 7A to 7C and FIG. 8, a board bending portion 18c as positioning means is provided at a longitudinal direction end of the conductive substrate 16. To



correspond to this, a fitting groove portion 18c' as positioning means in which said board bending portion 18c is fitted and engaged is comprised on the stay 13 side.

5           Bending processing 18c of this heater 17 can cope with not only an extension in the longitudinal direction of the heater 17 but also the revolution movement.

10           That is, although, usually, in the heater, when the recording material 11 at a room temperature enters in the fixing nip portion N, the temperature on the transferring upstream side becomes low, and for this reason, a warp is generated due to the thermal expansion difference between the upstream and  
15           downstream, as shown in FIG. 8, since the region in which the revolution movement can be done in the fitting gap to the fitting groove 18c' as the positioning means on the stay 13 side is regulated by one side standard, the movement on the electrodes 5  
20           side can be suppressed to 0.1 mm or less in which the wear due to sliding friction becomes no problem.

          Since a temperature difference of nearly 80°C is generated between the upstream and downstream of the usual heater, an extension difference of 0.23 mm is  
25           generated. This appears to be about 0.5 mm as a warp. In the conventional ceramic heater, since this is also distributed in the left and right and also in the

upstream and downstream, it is small as 0.125 mm, which becomes no problem. However, in case of completely

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stopping the extension on one side, a large displacement appears at a free end portion.

5 Accordingly, on the free end side, it is unsuitable for disposing an electrode.

To realize this embodiment, if the positioning means is one of the hole 18a as shown in FIGS. 3A to 3C and FIG. 4, if the clearance between the hole and the  
10 stay side is taken to be small as about 0.1 mm, the revolution movement can be regulated likewise, but, in this case, in order that the left and right are disposed symmetrically, the position of the positioning means 18a may be determined. However, in case of using  
15 the notch 18b as shown in FIGS. 5A to 5C and FIG. 6, ~~since there is no restriction force to the warp~~  
direction, it is unsuitable.

FIGS. 9A and 9B are model views showing shapes upon expansion of the heater 17 in the seat gouged  
20 portion 13a of the stay 13, in which FIG. 9A shows a case of the heater 17 in which the positioning means is the board bending portion 18c, and FIG. 9B shows a case of the heater 17 in which the positioning means is the hole 18a.

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25 (Embodiment 3)(FIGS. 10A to 10C and FIG. 11)

Although, in the embodiments 1 and 2, the electrodes 5 for power supply and the positioning means

18a, 18b and 18c are formed at the longitudinal direction end portions of the heater 17, it need not always be at end portions. As shown in FIGS. 10A to 10C and FIG. 11, even when the electrodes 5 and positioning means 18d are at the center, contact point defect can be prevented. In this case, since the thermal expansion of the heater 17 is distributed evenly in the longitudinal direction, the thermal distribution in the vertical direction to the paper-passing direction can be designed and realized symmetrically in the left and right.

In this case, since using the connecter as the above-described embodiment interferes with the film, power supply may be soldering of a lead line, or connected to the electrode by spot welding. Wiring of the lead line to the film guide can be freely designed if it does not obstruct sliding of the film.

(Others)

1) In a heating apparatus of a film heating system, an apparatus construction in which an endless belt-like film is wound and stretched by giving tension, and this is rotated and driven, is also possible. Besides, using an long ended film roll-wound, an apparatus construction is also possible so that this is run at a predetermined speed from the feeding-out axis side through the heater to the winding-up axis side.

2) Besides, it is of course that the heating body of the present invention can be applied to not only the heating apparatus of the film heating system but also a heating apparatus or the like in which a heating body supported by a heating body support body is directly contacted to a heated body and heated or the like.

3) Besides, it is of course that the heating apparatus of the present invention can be widely used as not only the image overheating fixing apparatus but also others, for example, an image heating apparatus in which a recording material carrying an image is heated and the surface property such as gloss is modified, an image heating apparatus which performs temporary fixing processing, a heating apparatus in which a sheet-like material is fed and dry processing and laminate processing are performed or the like.

The present invention is not limited to the above-described embodiments but includes modifications within its the scope of the preset invention.